

## INHIBITED OXIDATION OF CUMENE AND POLYMERIZATION OF STYRENE INVESTIGATED BY SOLUTION MICROCALORIMETRY

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### Abstract

The application of solution microcalorimetry was demonstrated on two model examples – inhibited oxidation of cumene and radical polymerization of styrene.

From the experimental dependences of the rate of heat release on time, the rate constants  $k_7$  of the interaction of an inhibitor with radicals of substrate ( $RO_2^{\cdot}$  or  $R^{\cdot}$ ) in oxidation or in polymerization were determined for the set of inhibitors of N-aryl N-(2-quinone) amine series. It was shown that these compounds are weak inhibitors of oxidation of cumene and rather efficient inhibitor of polymerization of styrene.

**Keywords:** cumene, oxidation, polymerization, quinone-amine inhibitors, solution microcalorimetry, styrene

### Introduction

Efficiency of inhibitors of polymerization of monomers and of oxidation of polymer materials and low molecular hydrocarbons may be tested by monitoring some elementary step of the free radical chain process involved either in initiation, propagation or termination stage of the reaction, which is affected by the presence of an inhibitor. Thus, DSC [1–4], thermogravimetry [5], ESR spectroscopy [6], chemiluminescence [7–16], oxygen absorption [17–20] and spectroscopy methods [21–23] for determination of reaction products can be used, the efficiency of the inhibitor is usually estimated from the inhibition period of oxidation. From this viewpoint, until now little attention has been paid to the solution microcalorimetry where the rate of the heat released ( $Q$ ) in the propagation stage of the reaction prevails the heat effects from other elementary reactions and thus it is directly proportional to the rate of oxidation or polymerization:

$$Q = \Delta H V w \quad (1)$$

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where,  $\Delta H$  is the reaction enthalpy,  $V$  is the volume of the reaction system and  $w$  is the rate of the reaction.

The method appears particularly suitable for investigation of the course of the inhibited chain radical reactions in oxidation of polymers and low molecular hydrocarbons [24] taking place in solutions. The oxidation of low molecular hydrocarbons like ethyl benzene, cumene and edible oils are the most representative examples.

In the present paper, the oxidation of cumene and polymerization of styrene initiated by 2,2-azobis(isobutyronitril)(AIBN), inhibited by the set of N-aryl N-2-(1,4-quinone) amines has been examined at 60°C using the Privalov's solution microcalorimeter. The inhibition pattern of the respective additive was investigated with the aim to determine the rate constant of transfer reaction of the chain propagating radicals to the inhibitor.

## Experimental

### *Procedure*

The rate of the heat release during inhibited oxidation of cumene and/or polymerization of styrene was measured by the calorimeter MKDP-2 produced at the Institute of Crude Oil Chemistry, Tomsk, Russia.

The solution of an inhibitor in the hydrocarbon (cumene and styrene) (4 ml) were introduced to the teflon reaction vessel of the overall volume 10 ml. Initiator was placed into the special open capsule floating on the surface of the liquid.

In oxidation studies, the solution has been bubbled through by oxygen and the reaction vessel was gas-tightly closed. In polymerization experiments, a special reaction vessel has been used enabling the degassing the system from oxygen in a repeated cycle of freezing and filling with nitrogen. The reaction vessel was placed in the measuring head of the calorimeter. When the system of reactants was thermostated to a given temperature the semiroating motion of calorimetric head provided the mixing and dissolution of initiator in the solution. The motion of the head was kept throughout the measurements.

### *Chemicals*

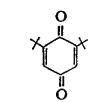
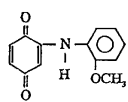
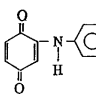
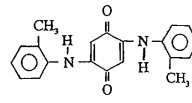
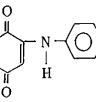
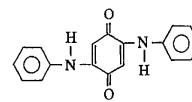
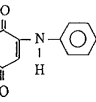
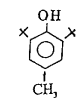
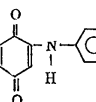
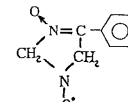
AIBN was used as the initiator of polymerization of styrene and oxidation of cumene. It was purified by two-fold recrystallization from ethanol.

Cumene was purified by extraction with concentrated  $H_2SO_4$ , with solution of NaOH, water and dried over  $Na_2CO_3$ , vacuum distilled and filtered through a column filled with activated  $Al_2O_3$ .

Styrene was purified with 5% water solution of NaOH, washed with water, dried over  $Na_2CO_3$  and vacuum distilled.

Structure of inhibitors used in both the oxidation and polymerization measurements is given in the Table 1. Substances 2–8 were synthesized and kindly supplied by the group of Schulz from the University Merseburg, Germany. Besides the compound 1 they all contain several reactive sites in one molecule. Benzoquinone moi-

**Table 1** Structure of the inhibitors studied

1		6	
2		7	
3		8	
4		9	
5		10	

ety of the inhibitor was assumed to provide an inhibiting effect in radical polymerization of vinyl monomers reacting with the growing alkyl radicals. Aromatic amine site of a molecule, on the other hand, reacts preferentially with peroxy radicals being formed in oxygen containing atmosphere during oxidation. Substituents on the phenyl ring (compounds 3, 4, 5, 6) performing electron donor ( $-\text{CH}_3$ ,  $-\text{OCH}_3$ ), or electron acceptor ( $-\text{Cl}$ ) effects as well as the unsubstituted compounds composed of one benzoquinone and two amine moieties (compounds 7 and 8) were expected to modify antioxidative efficiency of the inhibitors studied.

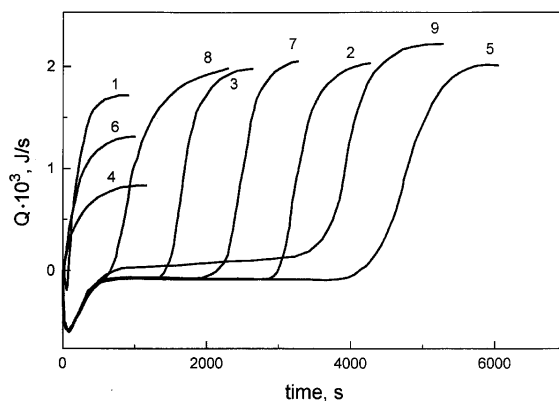
## Results and discussion

Illustrative plots of the rate of heat release on time for both the oxidation of cumene and polymerization of styrene at  $60^\circ\text{C}$  are given in the Figs 1 and 2.

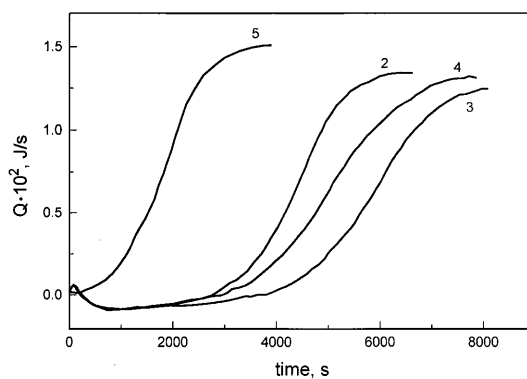
Some important statements follow from the experimental runs:

Dissolution of the initiator after the mixing of reactants is endothermic process. However, the line observed is retained on the endothermic side even in further stages of the process for both the inhibited oxidation and polymerization. Such effect of inhibitors, which appears to be quite typical for quinone amines, was not observed for phenols and aromatic amines. As it was reported in [24] and [25] these compounds gave the line which turned immediately to the exothermic side of the scale when initiator has been dissolved (e.g. the line 9 of Fig. 1 for 2,6-*di*-*tert*-butyl 4-methyl phenol).

For inhibited polymerization of styrene, the dependence of the value of this negative heat effect on the rate of initiation as well as on inhibitor concentration was followed. The plots of the maximum negative values of the heat release on the rate of

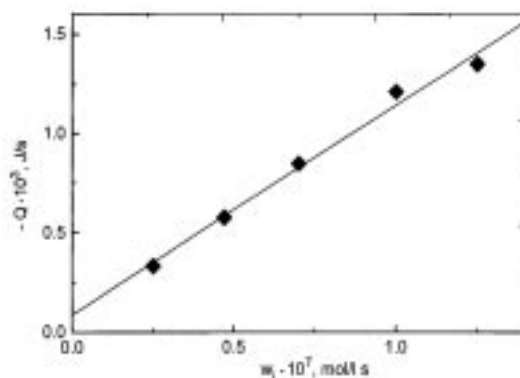


**Fig. 1** The plot of the rate of heat release  $Q$  vs. time  $t$  in oxidation of cumene inhibited by substances 1–9 from the Table 1. Initiator: AIBN;  $T=60^{\circ}\text{C}$ ;  $[\text{InH}]=2.5 \cdot 10^{-4} \text{ mol l}^{-1}$ ; The rate of initiation  $w_i=3.4 \cdot 10^{-8} \text{ mol l}^{-1} \text{ s}^{-1}$ ,  $w_i$  were calculated according to the relation  $w_i=ek[\text{AIBN}]$  where  $k=1.58 \cdot 10^{15} \exp(-30800/RT)$ ; Line 9 shows the effect of 2,6-*di*-*tert*-butyl-4-methyl-phenol (ionol); its initial concentration  $7 \cdot 10^{-5} \text{ mol l}^{-1}$

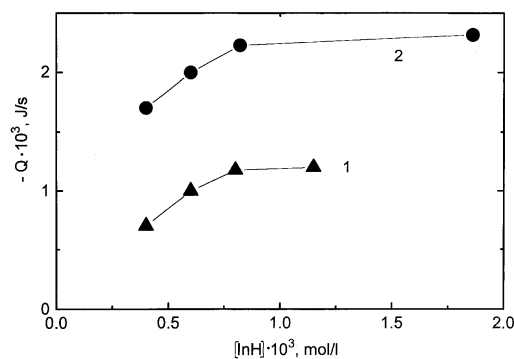


**Fig. 2** The plot of the heat release vs. time in the polymerization of styrene in the presence of inhibitors 2, 3, 4 and 5 from Table 1 at  $60^{\circ}\text{C}$ . Initiator: AIBN;  $[\text{InH}]=7.5 \cdot 10^{-4} \text{ mol l}^{-1}$ ,  $w_i=1.2 \cdot 10^{-7} \text{ mol l}^{-1} \text{ s}^{-1}$

initiation and initial concentration of inhibitors for the compounds 1 and 10 are shown in the Figs 3 and 4. The main process taking place during the inhibition period appears to be the reaction of growing macroradicals with the molecule of inhibitor. Since with the increase of the rate of initiation the stationary concentration of radicals  $R'$  increases too, this might explain the observed linearity between the negative values of the heat released (positive values of heat absorbed) and the rate of initiation. The increase of the negative value of the rate of heat release was observed also for the increase of the initial concentration of inhibitor added (Fig. 4), however, the curve declines from the linearity above the initial concentration of inhibitor:  $[\text{InH}] > 7.5 \cdot 10^{-4} \text{ mol l}^{-1}$ . This is explained by decreasing solubility of an inhibitor at its higher initial concentration.



**Fig. 3** The plot of the maximum rate of negative heat release in the inhibition period of polymerization of styrene vs. the rate of initiation. Initiator: AIBN;  $[\text{InH}]$  (Compound 1 from Table 1) =  $1 \cdot 10^{-3} \text{ mol l}^{-1}$ ;  $T=60^\circ\text{C}$



**Fig. 4** The plot of the maximum rate of negative heat release in the inhibition period of polymerization of styrene vs. concentration of inhibitors. Initiator: AIBN;  $w_i=1.2 \cdot 10^{-7} \text{ mol l}^{-1} \text{ s}^{-1}$ ;  $T=60^\circ\text{C}$ ; Line 1: InH 1; Line 2: InH 10

Experimental studies presented in Figs 1 and 2 thus provide an evidence of the endothermicity of the interaction of  $\text{R}^\cdot$  and  $\text{RO}_2^\cdot$  radicals with the set of inhibitors (the compounds 2–8, 10 in Table 1).

There are not available literature data on  $\Delta H$  values describing the interactions of peroxy radicals with compounds of Table 1. Handbook of Antioxidants [26], brings the data of  $\Delta H$  for the interaction of *tert*- $\text{RO}_2^\cdot$  with 4- $\text{NO}_2$  substituted diphenyl amine which is  $14.3 \text{ kJ mol}^{-1}$  while that for *sec*- $\text{RO}_2^\cdot$  it is  $7.4 \text{ kJ mol}^{-1}$ . One can suppose, that the endothermicity in a similar extent is valid also for the interaction of cumene peroxy radical with inhibitors 2–8, 10 of Table 1.

We have neglected the heat effects due to the initiation and termination reactions. Such an assumption is justified by the following calculations:

The rate of the heat release  $Q_i$  due to the initiation reaction should be:

$$Q_i = \Delta H_{\text{init}} V w_i \quad (2)$$

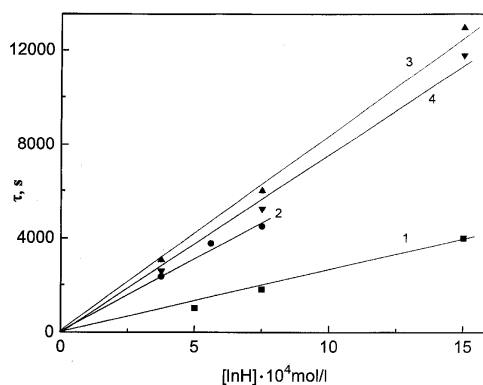
The rate of initiation in polymerization of styrene at 60°C is  $w_i = 1.2 \cdot 10^{-7} \text{ mol l}^{-1} \text{ s}^{-1}$  (calculated from the amount of initiator used, the rate constant of initiator decomposition and yield of radicals from the cage 0.8 [27]), the reaction volume  $V = 4 \cdot 10^{-3} \text{ l}$  and the heat of reaction  $\Delta H_{\text{init}}$  from [28] is  $131 \text{ kJ mol}^{-1}$ . Accordingly, the rate of the heat release calculated from these values should be  $6.28 \cdot 10^{-5} \text{ J s}^{-1}$ . Comparing it with the value of the heat release measured under the stationary conditions of polymerization of styrene ( $Q_{\text{stat}} = 1.5 \cdot 10^{-2} \text{ J s}^{-1}$ ),  $Q_i$  takes only 0.5% of  $Q_{\text{stat}}$ . For oxidation of cumene  $Q_i = 1.78 \cdot 10^{-5} \text{ J s}^{-1}$ , which is again lower than 1% of  $Q_{\text{stat}}$  (Figs 1 and 2).

The contribution of recombination reactions of alkyl or alkylperoxy radicals to the overall reaction heat can be estimated for the steady course of the reaction in which the rate of initiation equals to the rate of termination. The exothermicity of the termination reaction is about  $400 \text{ kJ mol}^{-1}$  for termination of  $\text{RO}_2$  radicals [29] and  $270\text{--}340 \text{ kJ mol}^{-1}$  for termination of alkyl radicals. In the oxidation or polymerization experiments, the only termination reaction is the reaction of either two peroxy radicals or the reaction of two growing polymerization alkyl radicals. The correction on the heat released in termination reactions can thus reach 3% of the stationary value of the heat measured in oxidation [24] and may be neglected, too.

In the first characterization of the inhibition efficiency, the induction period usually shows how long time a certain inhibitor withstands the attack of reactive free radicals and converts them to less reactive radicals.

As it is seen from the Figs 1 and 2 the inhibition period depends significantly on the character of substituted groups on the phenyl ring as well as on the initial concentration of inhibitors (Fig. 5). The plot of inhibition period vs. the initial concentration of inhibitor is essentially linear.

In oxidation of cumene, the most efficient inhibitor is compound 5 containing  $-\text{Cl}$  in the position 4 on phenyl ring of  $N$ -aryl  $N$ -(2-benzoquinone) amine. Ionol (compound 9) is slightly less efficient, followed by the compound 2 having unsubstituted phenyl ring and 7 which is 2,5-benzoquinone bis/ $N$ -(2-toluy) diamine.



**Fig. 5** The plot of inhibition times  $\tau$  for polymerization of styrene at 60°C vs. initial concentration of inhibitors 1–4 from Table 1. The rate of initiation  $w_i = 1.2 \cdot 10^{-7} \text{ l mol}^{-1} \text{ s}^{-1}$

Some efficiency is provided also by compound 3 and 8, which are nonsubstituted N-(2-benzoquinone) N-phenyl amine and corresponding benzoquinone diamine. It is of interest that substitution by methoxy group of phenyl ring either in position 2 or 4 leads practically to the total suppression of inhibition efficiency of benzoquinone amines. The inhibiting efficiency of 2,6-*ditert*-butyl benzoquinone in oxidation of cumene is also very weak. As it is evidenced by the lower value of  $Q_{stab}$ , the latter compounds act as retardants of oxidation.

In polymerization of styrene, the most efficient inhibitor appears to be compound 3 (benzoquinone aryl amine substituted by methyl group in position 4 on the phenyl ring), very efficient is also the substitution by methoxyl group in the position 4 on the phenyl ring (compound 4) and nonsubstituted benzoquinone aryl amine (compound 2). On the other hand, the substitution of the phenyl ring by chlorine provides only moderate efficiency in inhibition of polymerization of styrene.

The -Cl substitution on the phenyl ring of the inhibitor (compound 5 in Table 1) thus acts in an opposite way to -CH<sub>3</sub> substitution (compound 6) when oxidation of cumene and polymerization of styrene are compared. Inhibitor with chlorine atoms gives the higher inhibition period in oxidation of cumene when compared to -CH<sub>3</sub> substitution while in polymerization of styrene it is vice versa. According to [27], however, the reactivity of benzoquinone itself towards alkyl radicals during the polymerization decreases with increasing number of methyl groups in the molecule while the chlorine substitution leads to an increase of the quinone reactivity towards alkyl radicals. This discrepancy indicates that the primary attack of either peroxy radicals during oxidation or alkyl radicals during polymerization is preferably focused on amine group of respective quinone amine.

Inhibition time  $\tau$  is usually expressed as:

$$\tau = \frac{[\text{InH}]}{w_i} \quad (3)$$

where [InH] is molar concentration of an inhibitor and  $w_i$  is the rate of initiation. In the case of AIBN initiation  $w_i = 2k_d[\text{AIBN}]e$ , where  $k_d$  is the rate constant of AIBN decomposition, [AIBN] is molar concentration of AIBN and  $e = 0.8$  is the yield of radicals from the cage.

Induction times  $\tau$  obtained from the intersections of the straight line of the maximum slope passing through the inflection point and the base line of the time axis (Figs 1 and 2, Tables 2 and 3), however, do not follow exactly the above equation; the effective concentration of inhibitor corresponds very rarely to that calculated from the weighed amount of inhibitor InH. Its effective concentration [InH]<sub>eff</sub> can be approximated by the expression:

$$[\text{InH}]_{\text{eff}} = fn[\text{InH}], \quad (4)$$

where  $f$  is the number of inhibiting functions in one molecule of inhibitor and  $n$  is the number of reactive free radicals which can disappear due to one inhibiting function.

**Table 2** Experimentally determined and calculated parameters of initiated oxidation of cumene inhibited by inhibitors from the Table 1.

Concentration of inhibitor  $[\text{InH}] = 2.5 \cdot 10^{-4} \text{ mol l}^{-1}$  (compounds 1–8);  $[\text{InH}] = 7 \cdot 10^{-5} \text{ mol l}^{-1}$  (compound 9), the rate of initiation  $w_i = 3.4 \cdot 10^{-8} \text{ mol l}^{-1} \text{ s}^{-1}$

Comp. No.	$Q_{\text{stat}} \cdot 10^3 / \text{J s}^{-1}$	$\tau / \text{s}$	$k_7 / (fn) \cdot 10^{-3} / \text{mol}^{-1} \text{ s}^{-1}$		$fn$		$k_7 \cdot 10^{-4} / \text{mol}^{-1} \text{ s}^{-1}$
			$\alpha$	$\beta$	a	b	
1	1.75	83	7.7	18.5	–	0.03	0.023
2	2.10	3011	14.4	12.5	0.41	0.45	0.65
3	2.00	1476	12.8	13.0	0.20	0.24	0.31
4	0.85	23	2.9	–	–	0.03	0.009
5	2.05	4234	10.3	11.5	0.58	0.67	0.69
6	1.35	23	4.2	15.5	–	0.03	0.012
7	2.10	2276	12.7	11.4	0.31	0.34	0.39
8	2.00	726	9.2	6.8	0.10	0.14	0.13
9	2.25	3633	8.8	7.6	1.76	1.82	1.60 <sup>c)</sup>

a – calculated from induction time, presumed initiation rate and concentration of inhibitor  $[\text{InH}]$  according to Eqs (3) and (4)

b – calculated by non-linear regression analysis of observed curves comparing  $w_i$  and  $w_{\text{eff}}$  determined by fitting of theoretical curves to the experimental runs

c – value  $k_7$  from the previous paper is  $2.2 \cdot 10^4 \text{ l mol}^{-1} \text{ s}^{-1}$  [32]

$\alpha$  – determined by Bagdassaryan-Bamford method [30]

$\beta$  – determined by non-linear regression analysis

**Table 3** Parameters of polymerization of styrene inhibited by quinone amines from the Table 1. The concentration of inhibitor  $[\text{InH}] = 7.5 \cdot 10^{-4} \text{ mol l}^{-1}$ , the rate of initiation  $w_i = 1.2 \cdot 10^{-7} \text{ mol l}^{-1} \text{ s}^{-1}$ 

Comp. No.	$Q_{\text{stat}} \cdot 10^3 / \text{J s}^{-1}$	$\tau / \text{s}$	$k_7 / (fn) \cdot 10^{-3} / \text{mol}^{-1} \text{ s}^{-1}$		$fn$		$k_7 \cdot 10^{-4} / \text{mol}^{-1} \text{ s}^{-1}$
			$\alpha$	$\beta$	a	b	
2	14.0	3600	79.0	97.0	0.58	0.75	5.90
3	12.8	4700	67.0	102.0	0.78	0.98	6.56
4	14.0	3750	64.0	87.0	0.60	0.85	5.44
5	15.5	1000	53.0	114.0	0.16	0.32	1.70

a – calculated from induction time, presumed initiation rate and concentration of inhibitor  $[\text{InH}]$  according to Eqs (3) and (4)

b – calculated by non-linear regression analysis of observed curves comparing  $w_i$  and  $w_{\text{eff}}$  determined by fitting of theoretical curves to the experimental runs

$\alpha$  – determined by Bagdassaryan-Bamford method [30]

$\beta$  – determined by non-linear regression analysis

For example, one radical can react with amino group in transfer reaction giving a more stable N radical and the second one with this N radical in termination process.



The factors  $fn$  determined from the induction times and from the known rate of initiation are listed in the Tables 2 and 3 for both oxidation and polymerization experiment.

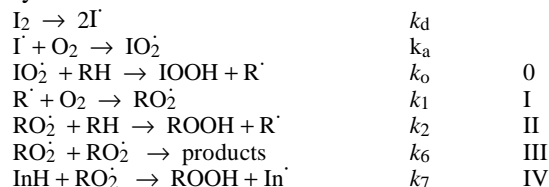
*Methods of evaluation of curves obtained and determination of the rate constant of the transfer of radicals to inhibitor*

The rate  $w$  of the two qualitatively different processes – thermooxidation and radical polymerization – measured by the solution calorimeter can be characterized formally by the identical equations:

$$w = k[\text{RH}][\text{P}'] \quad (5)$$

where  $k$  is the rate constant of the propagation step,  $[\text{RH}]$  is the concentration of the substrate and  $[\text{P}']$  denotes the concentration of propagating free radicals (peroxy radicals  $\text{RO}_2\dot{}$  in oxidation or  $\text{R}'$  growth polymerization radicals in polymerization).

Initiated oxidation of hydrocarbons in the presence of an inhibitor  $\text{InH}$  was described by the classical scheme:



Here,  $\text{I}'$  is the radical derived from initiator,  $\text{RH}$  is the hydrocarbon substrate,  $\text{R}'$  and  $\text{RO}_2\dot{}$  are alkyl and alkyl peroxy radicals,  $\text{InH}$  is inhibitor. As the reaction temperature was rather low, the thermal decomposition of hydroperoxides  $\text{IOOH}$  and  $\text{ROOH}$  does not contribute to the initiation reaction significantly.

First elementary reaction of radical polymerization is the addition of initiating radical to monomer molecule ( $\text{M}$ )



The elementary reactions in polymerization are formally identical with those of the above oxidation scheme I–IV;  $\text{RO}_2\dot{}$  radicals are replaced by  $\text{RM}'(\text{R}')$  radicals and instead of transfer reactions II and IV the addition reaction  $\text{R}' + \text{M} \rightarrow \text{R}'$  and transfer reaction  $\text{InH} + \text{R}' \rightarrow \text{In}' + \text{RH}$  take place.

In both cases of oxidation and polymerization, the presence of inhibitor leads to more or less efficient elimination of the propagation step depending on the value of the ratio  $k_7[\text{InH}]/k_2[\text{RH}]$  or  $k_7'[\text{InH}]/k_2'[\text{M}]$  ( $k_2'$  and  $k_7'$  are the rate constants of addition of growing polymerization radicals to monomer and transfer reaction to inhibitor, respectively), which determines the efficiency of the inhibitor. This is why the kinetic course of the process shows a rather distinct inhibition period. During this period, the inhibitor is steadily consumed and the rate of the process ultimately reaches the value as in its absence. The rate of the heat release on time performs thus typical sigmoidal shape.

Stationary conditions for inhibited oxidation and polymerization can be formally described by the identical equations:

$$w_i = k_6[\text{RO}_2^\cdot]^2 + k_7[\text{RO}_2^\cdot][\text{InH}] \quad (6)$$

$$w_i = k_6[\text{R}^\cdot]^2 + k_7[\text{R}^\cdot][\text{InH}] \quad (7)$$

where  $w_i$  is the initiation rate,  $k_6$  and  $k_7$  are the rate constants of termination and reaction of peroxy or alkyl radicals with an inhibitor.

When the inhibition period ends, the concentration of the inhibitor can be considered as zero. The Eqs (6) and (7) then have the form:

$$w_i = k_6[\text{RO}_{2\text{stat}}^\cdot]^2 \quad (8)$$

$$w_i = k_6[\text{R}_{\text{stat}}^\cdot]^2 \quad (9)$$

where  $[\text{RO}_{2\text{stat}}^\cdot]$  and  $[\text{R}_{\text{stat}}^\cdot]$  are stationary concentrations of peroxy and alkyl radicals. Substitution the Eqs (8) and (9) into Eqs (5) and (1) leads to the equations for the rate of the heat release when inhibitor InH has been consumed:

$$Q_{\text{stat}} = \frac{\Delta H V k_2 [\text{RH}] w_i^{1/2}}{k_6^{1/2}} \quad (10)$$

$$Q_{\text{stat}} = \frac{\Delta H V k_2 [\text{M}] w_i^{1/2}}{k_6^{1/2}} \quad (11)$$

Substitution of the concentration of peroxy  $\text{RO}_2^\cdot$  or alkyl  $\text{R}^\cdot$  radicals expressed from the Eqs (6) and (7), i.e.

$$[\text{RO}_2^\cdot] = \frac{-k_7[\text{InH}] + \sqrt{k_7^2[\text{InH}]^2 + 4w_i k_6}}{2k_6} \quad (12)$$

into Eq. (13),

$$Q_t = \Delta H V k_2 [\text{RH}] [\text{RO}_2^\cdot] \quad (13)$$

describes the rate of heat release in time  $t$ .

Two approaches for the estimation of kinetic parameter  $k_7$  of inhibitors were used:

a) Non-linear regression analysis, minimizing the sum of squares for experimental and theoretical courses. The latter were described by the function (13), using the expression (12) for which the concentration of inhibitor was found by parallel solution of the differential Eq. (14) in each iteration step.

$$\frac{d[\text{InH}]}{dt} = k_7[\text{RO}_2^\cdot][\text{InH}] \quad (14)$$

This enables to estimate the ratio  $k_7/\sqrt{k_6}$  as well as the effective rate of initiation  $w_{\text{eff}}$  and to compare it with the value of the initiation rate evaluated from the rate of decomposition of AIBN and thus to calculate the factor  $fn$ .

b) Graphical approach based on the experimentally determined ratio  $Q_t/Q_{\text{stat}}$  (modified Bamford-Bagdassaryan equation [30]) in the form:

$$-\frac{1}{\Phi} + \ln \frac{1 + \Phi}{1 - \Phi} = \frac{k_7 Q_{\text{stat}} t}{\Delta H V k_2 [\text{RH}]} + A_i \quad (15)$$

where

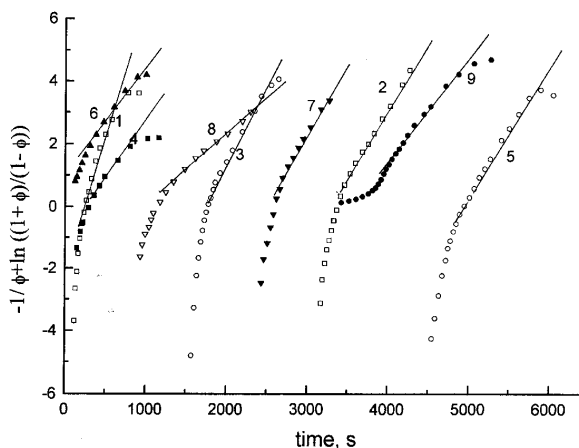
$$\Phi = \frac{Q_t}{Q_{\text{stat}}} \quad (16)$$

and  $A_i$  is a constant.

In Eq. (15), the Eqs (10)–(13) are combined with the analytical solution of Eq. (14).

The dependence of the left side of this equation on time  $t$  should be a straight line, from its slope the ratio  $k_7/k_2$  can be obtained. However, as it can be seen from the Bagdassaryan-Bamford transformation of the experimental curves for oxidation of cumene (Fig. 6), the linearity holds only for a limited section of the above graphs. This approach thus may involve some error in determination of the rate constant  $k_7$  depending on the selection of the proper part of the transformed line. By further analysis of Bagdassaryan-Bamford transformation we have found that the realistic values of the rate constant of inhibition are obtained when a steeply increasing part of the curve is involved in the evaluation.

From this viewpoint non-linear regression analysis of the experimental curves yields better coincidence with the theoretical assumption.



**Fig. 6** Bamford-Bagdassaryan metamorphosis of the lines 1–9 of Fig. 1 for the oxidation of cumene at 60°C

Provided that the rate constants  $k_6$  and  $k_2$  are available, the described procedure allows for the calculation of the rate constant of the inhibitor interaction with propagation free radicals ( $R\cdot$  or  $RO_2\cdot$ ) either in the case of oxidation of cumene or polymerization of styrene.

For determination of  $k_7$  constants for inhibited oxidation of cumene and polymerization of styrene the following parameters were used:

inhibited oxidation of cumene	inhibited polymerization of styrene
$k_6=1.9 \cdot 10^4 \text{ l mol}^{-1} \text{ s}^{-1}$ [31]	$k_6=7.2 \cdot 10^7 \text{ l mol}^{-1} \text{ s}^{-1}$ [31]
$k_2=1.75 \text{ l mol}^{-1} \text{ s}^{-1}$ [32]	$k_2=176 \text{ l mol}^{-1} \text{ s}^{-1}$ [31]
$V=4 \text{ ml}$	$V=4 \text{ ml}$
$[RH]=6.9 \text{ mol l}^{-1}$	$[RH]=8.26 \text{ mol l}^{-1}$
$\Delta H=114 \text{ kJ mol}^{-1}$	$\Delta H=67.3 \text{ kJ mol}^{-1}$
$Q_{\text{stat}}=\text{values in Tables 2 and 3}$	

The rate of initiation  $w_i$  was calculated using parameters for AIBN decomposition published in [27].

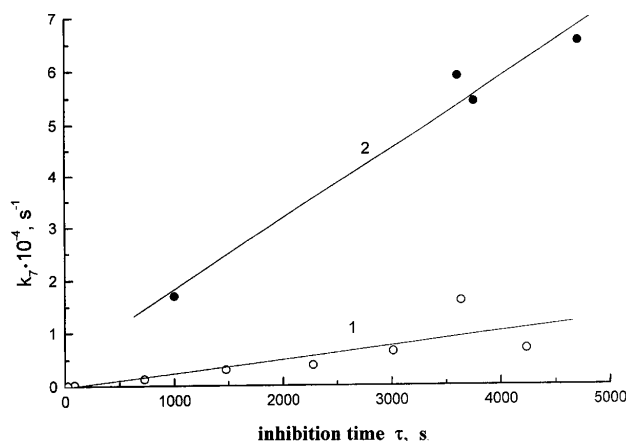


Fig. 7 Correlation between the rate constant  $k_7$  of inhibition for oxidation of cumene (line 1) and polymerization of styrene (line 2) at  $60^\circ\text{C}$

The values of  $k_7/(fn)$  for both the oxidation of cumene and polymerization of styrene which were obtained by the two approaches are presented in Tables 2 and 3. The correspondence between the values of  $k_7$  and inhibition time  $\tau$  is obvious (Fig. 7). It is worth of mentioning that the values of  $fn$  are lower than 1 for all benzoquinones examined for both the oxidation and polymerization. When compared to ionol for which  $fn$  is approximately 1.8, benzoquinone amines interacting either with peroxy radicals during oxidation or with alkyl radicals during polymerization yield free radicals potentially still capable of propagating the kinetic chains. It appears that benzoquinone amines are relatively good inhibitors of the polymerization of styrene (the transfer rate constant of alkyl radicals to the inhibitor is of the order  $10^4 \text{ l mol}^{-1} \text{ s}^{-1}$ ) while they act as relatively weak inhibitors of oxidation of cumene (the rate constant  $k_7$  is by one order lower than that in polymerization).

## Conclusions

1. The solution microcalorimetry proves to be an excellent method for the estimation of antioxidative efficiency of inhibitors in free radicals reactions of polymerization and oxidation.

2. The rate constants of elementary reactions of peroxy or alkyl radicals with inhibitors may thus be determined which are in a good agreement with the results obtained by other methods.

\* \* \*

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